

1.0 DESCRIPTION:

BEARING PRESSURES FOR RECTANGULAR FOOTINGS WITH BIAXIAL UPLIFT.

Purpose

The purpose of this calculation sheet is to solve for design parameters of a footing, which will result in easy design of footing. The footing is subject to axial load and bearing (biaxial moment). The footing can have a portion of their footing area that does not act in bearing.

The parameters calculated are:

- Combined Forces and Moment at centroid of footing.
- Soil bearing pressure.
- Maximum bearing pressure.
- Bearing pressure at remaining foundation corners.
- Location of line of zero pressure.
- Percentage of footing area acting in bearing.
- Factors of Security (Overturning and Sliding).

Assumptions

The following assumptions are made in the derivation of the results presented in this calculation sheet:

- The foundation is rectangular.
- The foundation behaves as a rigid body.
- The foundation has a planar stress distribution, and the location of zero pressure is therefore linear.
- The bearing pressure can only be compressive in nature, and there are no tensile bearing stresses.

Referees

- "*Bearing Pressures For Rectangular Footings With Biaxial Uplift*" by Kenneth E. Wilson. Journal of Bridge Engineering / February 1997.

Materials

- Steel Reinforcing Bars

$$f_y := 4200 \frac{\text{kgf}}{\text{cm}^2}$$

$$E := 2039 \frac{\text{kgf}}{\text{cm}^2}$$

- Concrete

$$f_c := 400 \frac{\text{kgf}}{\text{cm}^2}$$

$$E_c := 15100 \cdot \sqrt{f_c \cdot \frac{\text{kgf}}{\text{cm}^2}}$$

$$\gamma_c := 2.40 \frac{\text{tonnef}}{\text{m}^3}$$

- Soil

$$q_{\text{all}} := 3.1 \frac{\text{kgf}}{\text{cm}^2}$$

$$E_{\text{soil}} := 360 \frac{\text{kgf}}{\text{cm}^2}$$

$$\gamma_{\text{soil}} := 1.85 \cdot \frac{\text{tonnef}}{\text{m}^3}$$

$$c := 0 \frac{\text{kgf}}{\text{cm}^2}$$

$$\phi := 33 \text{deg}$$

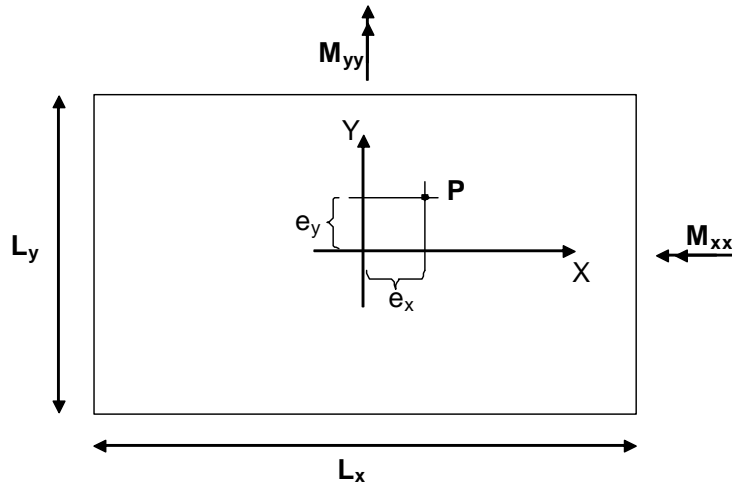
$$\nu_{\text{soil}} := 0.30$$

$$FS_{\text{sliding}}_{\text{all}} := 1.3$$

$$FS_{\text{OT}}_{\text{all}} := 1.4$$

$$\% \text{InContact}_{\text{all}} := 50\%$$

2.0 INPUT DATA:



- Length along X axis $L_x := 15\text{m}$
- Length along Y axis $L_y := 3\text{m}$
- Footing centroid $CG_x := 0\text{m}$
 $CG_y := 0\text{m}$
- Finish grade level $Grade := 4064.300\text{m}$
- Top of pedestal level $TOP := 4065.110\text{m}$
- Bottom of footing level $BOF := Grade - 1.7\text{m}$
- Thickness of footing $FootingThickness := 0.8\text{m}$
- FootingWeight := $\gamma_c \cdot FootingThickness \cdot L_x \cdot L_y$
- Soil thickness above footing $SoilAboveFooting := Grade - BOF - FootingThickness$
- SoilWeight := $\gamma_{soil} \cdot SoilAboveFooting \cdot L_x \cdot L_y$
- Total No of pedestals on the footing $NoOfPedestal := 3$
- Total No of loads $NoOfLoad := 8$
- Total No of load combinations $NoOfComb := 29$

Pedestal coordinates

Pedestal No.	Joint No.	Coordinates [m]	
		X	Y
1	1979	-6,00	0,00
2	1998	0,00	0,00
3	1981	6,00	0,00

Relocated footing centroid and pedestals

New pedestal coordinates:

$i := 0 \dots \text{NoOfPedestal} - 1$

Case #1

$$XY_{i,1} := XY_{i,1} - \frac{CG_x}{m}$$

$$XY_{i,2} := XY_{i,2} - \frac{CG_y}{m}$$

Case #2

$$L_{x,2} := L_y$$

$$L_{y,2} := L_x$$

$$CG_{x,2} := CG_y$$

$$CG_{y,2} := CG_x$$

Relocated footing centroid and pedestals

Loads on pedestal

Load	Joint No.	Forces [tonf]			Moments [tonf-m]	
		P	Vx	Vy	Mxx	Myy
DL	1979	-12,13	-0,59	0,31	-0,91	0,00
LL	1979	-1,71	-0,09	0,09	-0,28	0,00
ELx	1979	17,79	7,26	0,08	-0,17	0,00
Ely	1979	-3,04	-0,14	2,98	-13,85	0,00
WLx	1979	-1,68	-0,65	-0,01	0,01	0,00
WLy	1979	2,51	0,38	-2,74	12,95	0,00
SL	1979	-23,97	-1,32	1,22	-3,85	0,00
CL	1979	-3,27	0,02	0,36	-0,83	0,00
DL	1998	-12,43	0,00	0,31	-0,91	0,00
LL	1998	-1,72	0,00	0,09	-0,28	0,00
ELx	1998	0,00	14,22	0,06	0,00	0,00
Ely	1998	-2,75	-0,03	3,02	-14,06	0,00
WLx	1998	0,10	-1,31	-0,01	0,00	0,00
WLy	1998	4,69	0,03	-2,42	11,45	0,00
SL	1998	-24,12	-0,01	1,23	-3,86	0,00
CL	1998	-0,23	0,24	0,02	-0,07	0,00
DL	1981	-12,13	0,59	0,31	-0,91	0,00
LL	1981	-1,71	0,09	0,09	-0,28	0,00
ELx	1981	-17,79	7,26	-0,01	0,16	0,00
Ely	1981	-3,01	0,12	2,98	-13,85	0,00
WLx	1981	1,60	-0,66	0,00	-0,01	0,00
WLy	1981	2,48	-0,36	-2,74	12,96	0,00
SL	1981	-23,97	1,31	1,23	-3,85	0,00
CL	1981	-0,15	0,08	0,01	-0,04	0,00

Note : a) joint numbers are SAP2000 model nodes.

b) for establishing coordinates of the pedestals refer to previous page.

c) footing, pedestal and soil weight are not included.

Combination factors

Comb	Loads							
	DL	LL	ELx	ELy	WLx	WLy	SL	CL
1	1,00							
2	1,00	1,00						
3	1,00						1,00	
4	1,00				1,00			
5	1,00					1,00		
6	1,00		1,00					
7	1,00			1,00				
8	1,00		-1,00					
9	1,00			-1,00				
10	1,00	0,75			0,75		0,75	
11	1,00	0,75				0,75	0,75	
12	1,00	0,75	0,75				0,75	
13	1,00	0,75		0,75			0,75	
14	1,00	0,75	-0,75				0,75	
15	1,00	0,75		-0,75			0,75	
16	0,60				1,00			
17	0,60					1,00		
18	0,60		1,00					
19	0,60			1,00				
20	0,60		-1,00					
21	0,60			-1,00				
22	1,00	1,00						1,00
23	1,00						1,00	1,00
24	0,75	0,75			0,75		0,75	0,75
25	0,75	0,75				0,75	0,75	0,75
26	0,75	0,75	0,75				0,75	0,75
27	0,75	0,75		0,75			0,75	0,75
28	0,75	0,75	-0,75				0,75	0,75
29	0,75	0,75		-0,75			0,75	0,75

where,

- DL : dead load
- LL : live load
- CL : crane load
- WL : wind load
- EL : earthquake load

▣ Pedestal data

NoOfForce := cols(MatrixLoad) NoOfCoord := cols(XY)

MatrixXY := for i ∈ 0..NoOfComb - 1
 for j ∈ 0..NoOfCoord - 1
 for k ∈ 0..NoOfPedestal - 1
 MatrixXY._{i+NoOfComb·k,j} ← XY_{k,j}

Comb_{AUX} := for k ∈ 0..NoOfPedestal - 1
 Comb_{AUX}_{k,0} ← Comb

MatrixComb := for i ∈ 0..NoOfComb - 1
 for k ∈ 0..NoOfPedestal - 1
 MatrixComb._{i+NoOfComb·k} ← (Comb_{AUX}_{k,0})_i

CombFactor_{AUX} := for k ∈ 0..NoOfPedestal - 1
 CombFactor_{AUX}_{k,0} ← CombFactor

MatrixCombFactor := for i ∈ 0..NoOfComb - 1
 for j ∈ 0..NoOfLoad - 1
 for k ∈ 0..NoOfPedestal - 1
 MatrixCombFactor._{i+NoOfComb·k,j} ← (CombFactor_{AUX}_{k,0})_{i,j}

CombLoad_{AUX} := for k ∈ 0..NoOfPedestal - 1
 CombLoad_{AUX}_{k,0} ← CombFactor·submatrix[MatrixLoad, NoOfLoad·k, NoOfLoad·(k + 1)]

MatrixCombLoad := for i ∈ 0..NoOfComb - 1
 for j ∈ 0..NoOfForce - 1
 for k ∈ 0..NoOfPedestal - 1
 MatrixCombLoad._{i+NoOfComb·k,j} ← (CombLoad_{AUX}_{k,0})_{i,j}

MatrixLoad := $\left\{ \begin{array}{l} \text{MatrixLoad} \leftarrow \text{stack}(\text{MatrixComb}^T, \text{MatrixXY}^T, \text{MatrixCombLoad}^T) \\ \text{MatrixLoad} \leftarrow \text{MatrixLoad}^T \\ \text{csort}(\text{MatrixLoad}, 0) \end{array} \right.$

- Combined loads at the pedestals

Case #1		Coordinates [m]		Forces [tonf]			Moments [tonf-m]	
Comb	Joint No	X	Y	P	Vx	Vy	Mxx	Myy
1	1998	0,00	0,00	-12,43	0,00	0,31	-0,91	0,00
1	1981	6,00	0,00	-12,13	0,59	0,31	-0,91	0,00
1	1979	-6,00	0,00	-12,13	-0,59	0,31	-0,91	0,00
2	1998	0,00	0,00	-14,16	0,00	0,40	-1,18	0,00
2	1981	6,00	0,00	-13,84	0,68	0,40	-1,18	0,00
2	1979	-6,00	0,00	-13,84	-0,69	0,39	-1,18	0,00
3	1981	6,00	0,00	-36,09	1,90	1,54	-4,76	0,00
3	1979	-6,00	0,00	-36,10	-1,91	1,53	-4,76	0,00
3	1998	0,00	0,00	-36,55	-0,01	1,54	-4,77	0,00
4	1979	-6,00	0,00	-13,81	-1,24	0,30	-0,90	0,00
4	1998	0,00	0,00	-12,33	-1,31	0,30	-0,91	0,00
4	1981	6,00	0,00	-10,53	-0,08	0,31	-0,92	0,00
5	1979	-6,00	0,00	-9,62	-0,21	-2,44	12,05	0,00
5	1981	6,00	0,00	-9,65	0,23	-2,43	12,05	0,00
5	1998	0,00	0,00	-7,75	0,03	-2,11	10,54	0,00
6	1981	6,00	0,00	-29,92	7,85	0,30	-0,75	0,00
6	1998	0,00	0,00	-12,43	14,22	0,37	-0,91	0,00
6	1979	-6,00	0,00	5,66	6,67	0,38	-1,07	0,00
7	1979	-6,00	0,00	-15,17	-0,74	3,28	-14,76	0,00
7	1998	0,00	0,00	-15,18	-0,03	3,33	-14,96	0,00
7	1981	6,00	0,00	-15,14	0,71	3,29	-14,76	0,00
8	1998	0,00	0,00	-12,43	-14,23	0,24	-0,91	0,00
8	1979	-6,00	0,00	-29,92	-7,85	0,23	-0,74	0,00

$k := 0 \dots \text{NoOfPedestal} \cdot \text{NoOfComb} - 1$

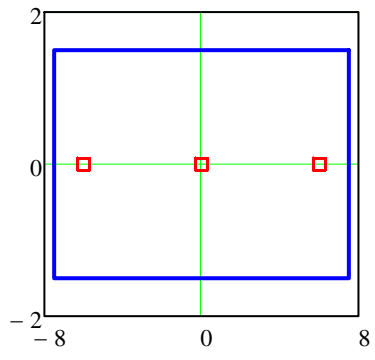
Case #1

$$XY_{\text{foot}} := \begin{pmatrix} 0.5 \cdot L_x & 0.5 \cdot L_y \\ -0.5 \cdot L_x & 0.5 \cdot L_y \\ -0.5 \cdot L_x & -0.5 \cdot L_y \\ 0.5 \cdot L_x & -0.5 \cdot L_y \\ 0.5 \cdot L_x & 0.5 \cdot L_y \end{pmatrix}$$

Case #2

$$XY_{\text{foot}.2} := \begin{pmatrix} 0.5 \cdot L_{x.2} & 0.5 \cdot L_{y.2} \\ -0.5 \cdot L_{x.2} & 0.5 \cdot L_{y.2} \\ -0.5 \cdot L_{x.2} & -0.5 \cdot L_{y.2} \\ 0.5 \cdot L_{x.2} & -0.5 \cdot L_{y.2} \\ 0.5 \cdot L_{x.2} & 0.5 \cdot L_{y.2} \end{pmatrix}$$

 Pedestal data



3.0 CALCULATIONS:

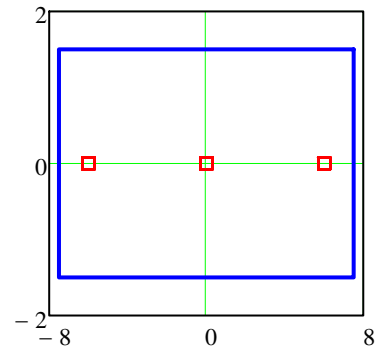
☑ Calculations

The footing dimensions must be assigned as L_x and L_y such that $\frac{e_y}{L_y} < \frac{e_x}{L_x}$

- Pedestal positions

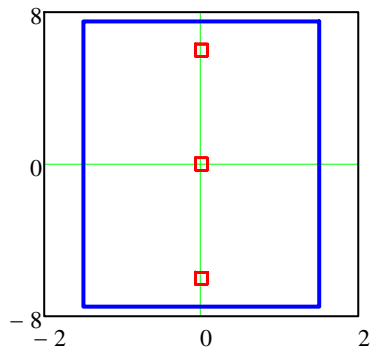
Case #1

$X := X \cdot m$ $Y := Y \cdot m$



Case #2 (90 degrees rotation about axes Z)

$X_2 := -Y$ $Y_2 := X$



- Forces (axial loads, shears and moments) acting on the pedestals

$$P_o := P_o \cdot \text{tonnef} \quad V_{ox} := V_{ox} \cdot \text{tonnef} \quad V_{oy} := V_{oy} \cdot \text{tonnef} \quad M_{ox} := M_{ox} \cdot \text{tonnef} \cdot \text{m} \quad M_{oy} := M_{oy} \cdot \text{tonnef} \cdot \text{m}$$

$$j := 0 \dots \text{NoOfComb} - 1$$

- Axial force at centroid of footing

$$P_j := \sum_{i=0+\text{NoOfPedestal} \cdot j}^{\text{NoOfPedestal} \cdot (j+1) - 1} P_{o_i} + (\text{FootingWeight} + \text{SoilWeight}) \cdot \text{CombFactor}_{j,0}$$

- Shear along X axis at centroid of footing

$$V_{x_j} := \sum_{i=0+\text{NoOfPedestal} \cdot j}^{\text{NoOfPedestal} \cdot (j+1) - 1} V_{ox_i}$$

- Shear along Y axis at centroid of footing

$$V_{y_j} := \sum_{i=0+\text{NoOfPedestal} \cdot j}^{\text{NoOfPedestal} \cdot (j+1) - 1} V_{oy_i}$$

- Moment about X axis at centroid of footing

$$M_{xx_j} := \sum_{i=0+\text{NoOfPedestal} \cdot j}^{\text{NoOfPedestal} \cdot (j+1) - 1} M_{ox_i} + \sum_{i=0+\text{NoOfPedestal} \cdot j}^{\text{NoOfPedestal} \cdot (j+1) - 1} (P_{o_i} \cdot Y_i) \dots$$

$$+ \sum_{i=0+\text{NoOfPedestal} \cdot j}^{\text{NoOfPedestal} \cdot (j+1) - 1} [V_{oy_i} \cdot (\text{TOP} - \text{BOF})]$$

- Moment about Y axis at centroid of footing

$$M_{yy,j} := \sum_{i=0+\text{NoOfPedestal}\cdot j}^{\text{NoOfPedestal}\cdot(j+1)-1} M_{oy,i} + \sum_{i=0+\text{NoOfPedestal}\cdot j}^{\text{NoOfPedestal}\cdot(j+1)-1} (P_{o,i} \cdot X_i) \dots$$

$$+ \sum_{i=0+\text{NoOfPedestal}\cdot j}^{\text{NoOfPedestal}\cdot(j+1)-1} [V_{ox,i} \cdot (\text{TOP} - \text{BOF})]$$

Case #2 (90 degrees rotation about axes Z)

$$P_{2,j} := P_j \quad V_{x,2,j} := -V_{y,j} \quad V_{y,2,j} := V_{x,j} \quad M_{xx,2,j} := M_{yy,j} \quad M_{yy,2,j} := -M_{xx,j}$$

- Corners in bearing

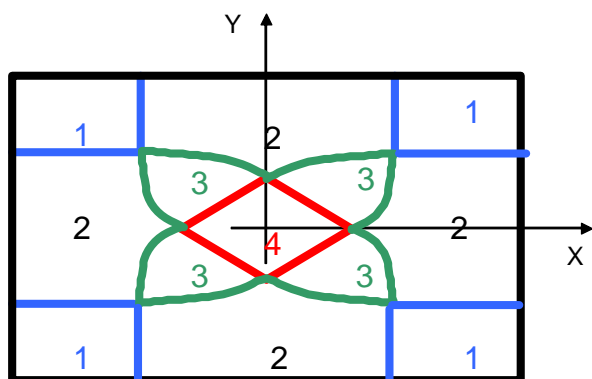
Case #1

$$e_{x,j} := \left| \frac{M_{yy,j}}{P_j} \right| \quad e_{y,j} := \left| \frac{M_{xx,j}}{P_j} \right|$$

Case #2 (90 degrees rotation about axes Z)

$$e_{x,2,j} := \left| \frac{M_{yy,2,j}}{P_{2,j}} \right| \quad e_{y,2,j} := \left| \frac{M_{xx,2,j}}{P_{2,j}} \right|$$

$$\text{Check}_j := \text{if} \left(\left| \frac{e_{y,j}}{L_y} \right| < \left| \frac{e_{x,j}}{L_x} \right|, \text{"Case #1"}, \text{"Case #2"} \right)$$



$$\text{NBC}_j := b(a) \leftarrow \frac{\frac{1}{6} - \frac{a^2}{6} + \frac{a^3}{12}}{1 - a + \frac{a^2}{3}}$$

$$\text{tope}_y \leftarrow b \left(4 \cdot \frac{e_x}{L_x} \right) \cdot L_y$$

$$\text{tope}_x \leftarrow b \left(4 \cdot \frac{e_y}{L_y} \right) \cdot L_x$$

$$\text{tope}_{y.2} \leftarrow b \left(4 \cdot \frac{e_{x.2}}{L_{x.2}} \right) \cdot L_{y.2}$$

$$\text{tope}_{x.2} \leftarrow b \left(4 \cdot \frac{e_{y.2}}{L_{y.2}} \right) \cdot L_{x.2}$$

$$\text{if } \left| \frac{e_{y_j}}{L_y} \right| < \left| \frac{e_{x_j}}{L_x} \right|$$

$$3 \text{ if } e_{x_j} \leq \text{tope}_{x_j} \wedge e_{y_j} \leq \text{tope}_{y_j} \wedge e_{y_j} > -\frac{L_y}{L_x} \cdot e_{x_j} + \frac{L_y}{6}$$

$$4 \text{ if } e_{y_j} \leq -\frac{L_y}{L_x} \cdot e_{x_j} + \frac{L_y}{6}$$

$$1 \text{ if } e_{y_j} \geq \frac{L_y}{4} \wedge e_{x_j} \geq \frac{L_x}{4}$$

2 otherwise

otherwise

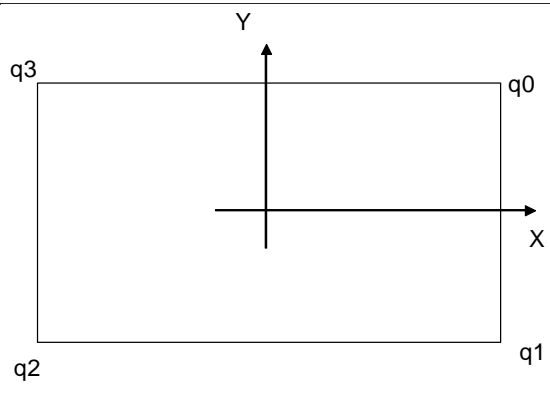
$$3 \text{ if } e_{x.2_j} \leq \text{tope}_{x.2_j} \wedge e_{y.2_j} \leq \text{tope}_{y.2_j} \wedge e_{y.2_j} > -\frac{L_{y.2}}{L_{x.2}} \cdot e_{x.2_j} + \frac{L_{y.2}}{6}$$

$$4 \text{ if } e_{y.2_j} \leq -\frac{L_{y.2}}{L_{x.2}} \cdot e_{x.2_j} + \frac{L_{y.2}}{6}$$

$$1 \text{ if } e_{y.2_j} \geq \frac{L_{y.2}}{4} \wedge e_{x.2_j} \geq \frac{L_{x.2}}{4}$$

2 otherwise

- Bearing pressures



$$A := L_x \cdot L_y$$

FOUR CORNERS IN BEARING

$q_{4CB} := \text{for } j \in 0 \dots \text{NoOfComb} - 1$

if $\left| \frac{e_{y,j}}{L_y} \right| < \left| \frac{e_{x,j}}{L_x} \right|$

$$q_{4CB_{0,j}} \leftarrow \frac{P_j}{A} \cdot \left(1 + \frac{6 \cdot e_{x,j}}{L_x} + \frac{6 \cdot e_{y,j}}{L_y} \right)$$

$$q_{4CB_{1,j}} \leftarrow \frac{P_j}{A} \cdot \left(1 + \frac{6 \cdot e_{x,j}}{L_x} - \frac{6 \cdot e_{y,j}}{L_y} \right)$$

$$q_{4CB_{2,j}} \leftarrow \frac{P_j}{A} \cdot \left(1 - \frac{6 \cdot e_{x,j}}{L_x} - \frac{6 \cdot e_{y,j}}{L_y} \right)$$

$$q_{4CB_{3,j}} \leftarrow \frac{P_j}{A} \cdot \left(1 - \frac{6 \cdot e_{x,j}}{L_x} + \frac{6 \cdot e_{y,j}}{L_y} \right)$$

otherwise

$$q_{4CB_{0,j}} \leftarrow \frac{P_{2j}}{A} \cdot \left(1 + \frac{6 \cdot e_{x,2j}}{L_{x,2}} + \frac{6 \cdot e_{y,2j}}{L_{y,2}} \right)$$

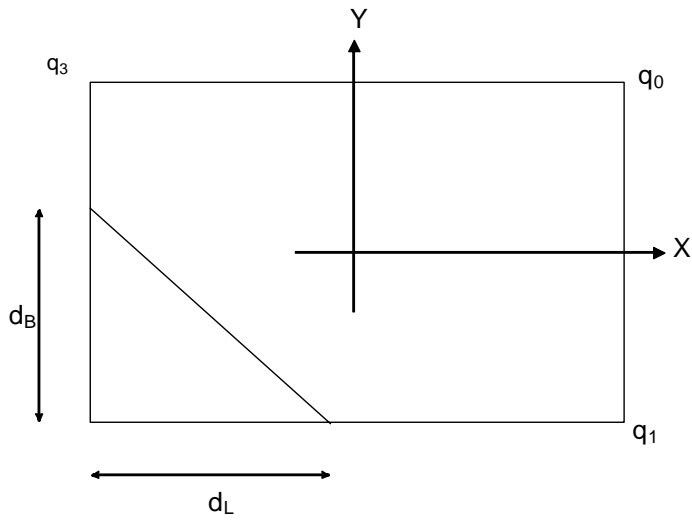
$$q_{4CB_{1,j}} \leftarrow \frac{P_{2j}}{A} \cdot \left(1 + \frac{6 \cdot e_{x,2j}}{L_{x,2}} - \frac{6 \cdot e_{y,2j}}{L_{y,2}} \right)$$

$$q_{4CB_{2,j}} \leftarrow \frac{P_{2j}}{A} \cdot \left(1 - \frac{6 \cdot e_{x,2j}}{L_{x,2}} - \frac{6 \cdot e_{y,2j}}{L_{y,2}} \right)$$

$$q_{4CB_{3,j}} \leftarrow \frac{P_{2j}}{A} \cdot \left(1 - \frac{6 \cdot e_{x,2j}}{L_{x,2}} + \frac{6 \cdot e_{y,2j}}{L_{y,2}} \right)$$

$\%A_{4CB_j} := 100\%$

THREE CORNERS IN BEARING



Given

$$0.5 \cdot (d_y - L_y) \cdot \left[\frac{0.5 \cdot d_x^2 \cdot (L_y - d_y)^2}{d_x \cdot (L_y - d_y) + L_x \cdot d_y} \right] + \left[0.5 \cdot L_y - \frac{5}{8} \cdot (L_y - d_y) \right] \cdot \left[\frac{\frac{1}{3} \cdot d_x^2 \cdot (L_y - d_y)^2 \cdot \frac{L_y - d_y}{d_y}}{d_x \cdot (L_y - d_y) + L_x \cdot d_y} \right]$$

$$\left[\frac{0.5 \cdot d_x^2 \cdot (L_y - d_y)^2}{d_x \cdot (L_y - d_y) + L_x \cdot d_y} \right] + \left[\frac{\frac{1}{3} \cdot d_x^2 \cdot (L_y - d_y)^2 \cdot \frac{L_y - d_y}{d_y}}{d_x \cdot (L_y - d_y) + L_x \cdot d_y} \right] + \left[\frac{L_y \cdot d_x \cdot (L_y - d_y) \cdot \left(L_x - L_y \cdot \frac{d_x}{d_y} \right)}{d_x \cdot (L_y - d_y) + L_x \cdot d_y} \right] + \left[\frac{0.5 \cdot L_y \cdot (L_x \cdot d_y - d_x \cdot L_x)}{d_x \cdot (L_y - d_y) + L_x \cdot d_y} \right]$$

$$0.5 \cdot \left[-L_x + d_x + \frac{4}{3} \cdot (L_y - d_y) \cdot \frac{d_x}{d_y} \right] \cdot \left[\frac{0.5 \cdot d_x^2 \cdot (L_y - d_y)^2}{d_x \cdot (L_y - d_y) + L_x \cdot d_y} \right] + \left[-0.5 \cdot L_x + \frac{3}{8} \cdot (L_y - d_y) \cdot \frac{d_x}{d_y} \right] \cdot \left[\frac{\frac{1}{3} \cdot d_x^2 \cdot (L_y - d_y)^2 \cdot \frac{L_y}{d_y}}{d_x \cdot (L_y - d_y) + L_x \cdot d_y} \right]$$

$$\left[\frac{0.5 \cdot d_x^2 \cdot (L_y - d_y)^2}{d_x \cdot (L_y - d_y) + L_x \cdot d_y} \right] + \left[\frac{\frac{1}{3} \cdot d_x^2 \cdot (L_y - d_y)^2 \cdot \frac{L_y - d_y}{d_y}}{d_x \cdot (L_y - d_y) + L_x \cdot d_y} \right] + \left[\frac{L_y \cdot d_x \cdot (L_x - L_y \cdot \frac{d_x}{d_y})}{d_x \cdot (L_y - d_y) + L_x \cdot d_y} \right]$$

$$0 \text{ cm} < d_x < L_x$$

$$0 \text{ cm} < d_y < L_y$$

$$\text{eqn}_3(L_x, L_y, d_x, d_y, ex, ey) := \text{Find}(d_x, d_y)$$

$$q_{3CB}(L_x, L_y, d_x, d_y, N, e_x, e_y) := \begin{cases} \begin{pmatrix} d_{x3} \\ d_{y3} \end{pmatrix} \leftarrow \text{eqn}_3(L_x, L_y, d_x, d_y, e_x, e_y) \\ K \leftarrow \frac{L_x \cdot d_{x3} \cdot d_{y3} \cdot (L_y - d_{y3}) + d_{x3}^2 \cdot (L_y - d_{y3})^2 \cdot \left(\frac{1}{3} + \frac{1}{6} \cdot \frac{d_{y3}}{L_y}\right) + (L_x \cdot d_{y3} - L_y \cdot d_{x3}) \cdot \left[\frac{1}{2} \cdot (L_x \cdot d_{y3} + L_y \cdot d_{x3})\right]}{d_{x3} \cdot (L_y - d_{y3}) + L_x \cdot d_{y3}} \\ q_{3CB} \leftarrow K \cdot \frac{N}{A} \cdot \begin{bmatrix} 1 \\ \frac{d_{y3} \cdot (L_x - d_{x3})}{d_{x3} \cdot (L_y - d_{y3}) + L_x \cdot d_{y3}} \\ 0 \\ \frac{d_{x3} \cdot (L_y - d_{y3})}{d_{x3} \cdot (L_y - d_{y3}) + L_x \cdot d_{y3}} \end{bmatrix} \\ \begin{pmatrix} d_{x3} \\ d_{y3} \end{pmatrix} \leftarrow \text{eqn}_3(L_x, L_y, d_x, d_y, e_x, e_y) \\ \%A_{3CB} \leftarrow \frac{A - 0.5 \cdot d_{x3} \cdot d_{y3}}{A} \end{cases}$$

$q_{3CB} := \text{for } i \in 0..3$

$\text{for } j \in 0.. \text{NoOfComb} - 1$

$\text{if } NBC_j = 3$

$\text{if } \left| \frac{e_{y,j}}{L_y} \right| < \left| \frac{e_{x,j}}{L_x} \right|$

$q_{aux} \leftarrow q_{3CB}(L_x, L_y, 1 \cdot \text{mm}, 1 \cdot \text{mm}, P_j, e_{x,j}, e_{y,j})$

$q_{i,j} \leftarrow q_{aux_{i,0}}$

otherwise

$q_{aux} \leftarrow q_{3CB}(L_{x,2}, L_{y,2}, 1 \cdot \text{mm}, 1 \cdot \text{mm}, P_j, e_{x,2j}, e_{y,2j})$

$q_{i,j} \leftarrow q_{aux_{i,0}}$

otherwise

$q_{aux} \leftarrow (0 \ 0 \ 0 \ 0)^T \cdot \frac{\text{kgf}}{\text{cm}^2}$

$q_{i,j} \leftarrow q_{aux_{i,0}}$

```
%A3CB := for j ∈ 0..NoOfComb - 1
```

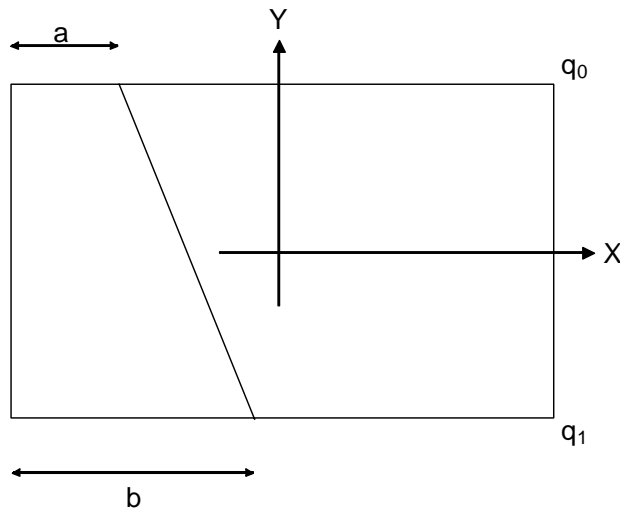
```
  if NBCj = 3
```

```
    %Aj ← %A3CB(Lx, Ly, 1mm, 1mm, ex,j, ey,j) if  $\left| \frac{e_{y,j}}{L_y} \right| < \left| \frac{e_{x,j}}{L_x} \right|$ 
```

```
    %Aj ← %A3CB(Lx,2, Ly,2, 1mm, 1mm, ex,2,j, ey,2,j) otherwise
```

```
  %Aj ← 0% otherwise
```


TWO CORNERS IN BEARING



Given

$$\frac{\frac{L_y}{6} \left[\frac{0.5 \cdot L_y \cdot (L_x - b_2) \cdot (b_2 - a_2)}{L_x - a_2} \right] + \frac{L_y}{4} \left[\frac{\frac{1}{6} \cdot L_y \cdot (b_2 - a_2)^2}{L_x - a_2} \right]}{\left[\frac{0.5 \cdot L_y \cdot (L_x - b_2)^2}{L_x - a_2} \right] + \left[\frac{0.5 \cdot L_y \cdot (L_x - b_2) \cdot (b_2 - a_2)}{L_x - a_2} \right] + \left[\frac{\frac{1}{6} \cdot L_y \cdot (b_2 - a_2)^2}{L_x - a_2} \right]} - e_y = 0 \cdot \text{cm}$$

$$\left(\frac{a_2}{2} - \frac{b_2}{6} + \frac{L_x}{6} \right) \cdot \left[\frac{0.5 \cdot L_y \cdot (L_x - b_2)^2}{L_x - a_2} \right] + \left(\frac{L_x}{2} - \frac{b_2 - a_2}{3} \right) \cdot \left[\frac{0.5 \cdot L_y \cdot (L_x - b_2) \cdot (b_2 - a_2)}{L_x - a_2} \right] + \left(\frac{L_x}{2} - \frac{b_2 - a_2}{4} \right) \cdot \left[\frac{\frac{1}{6} \cdot L_y \cdot (b_2 - a_2)^2}{L_x - a_2} \right]$$

$$0 \text{cm} < a_2 < L_x$$

$$0 \text{cm} < b_2 < L_x$$

$$\text{eqn}_2(L_x, L_y, a_2, b_2, e_x, e_y) := \text{Minerr}(a_2, b_2)$$

$$q_{2CB}(L_x, L_y, a_2, b_2, N, ex, ey) := \begin{cases} \begin{pmatrix} a_2 \\ b_2 \end{pmatrix} \leftarrow eqn_2(L_x, L_y, a_2, b_2, ex, ey) \\ K \leftarrow \frac{2 \cdot L_x \cdot (L_x - a_2)}{L_x^2 - L_x \cdot a_2 - L_x \cdot b_2 + \frac{1}{3} \cdot (a_2^2 + a_2 \cdot b_2 + b_2^2)} \\ q_{3CB} \leftarrow K \cdot \frac{N}{A} \cdot \begin{pmatrix} 1 \\ \frac{L_x - b_2}{L_x - a_2} \\ 0 \\ 0 \end{pmatrix} \end{cases}$$

$$\%A_{2CB}(L_x, L_y, a_2, b_2, ex, ey) := \begin{cases} \begin{pmatrix} a_2 \\ b_2 \end{pmatrix} \leftarrow eqn_2(L_x, L_y, a_2, b_2, ex, ey) \\ \frac{A - 0.5 \cdot (a_2 + b_2) \cdot L_y}{A} \end{cases}$$

```

q2CB := for i ∈ 0..3
  for j ∈ 0..NoOfComb - 1
    if NBC_j = 2
      if  $\left| \frac{e_{y,j}}{L_y} \right| < \left| \frac{e_{x,j}}{L_x} \right|$ 
        qaux ← q2CB(L_x, L_y, 1·mm, 1·mm, P_j, e_{x,j}, e_{y,j})
        q_{i,j} ← qaux_{i,0}
      otherwise
        qaux ← q2CB(L_{x,2}, L_{y,2}, 1·mm, 1·mm, P_{2,j}, e_{x,2,j}, e_{y,2,j})
        q_{i,j} ← qaux_{i,0}
    otherwise
      qaux ← (0 0 0 0)T ·  $\frac{\text{kgf}}{\text{cm}^2}$ 
      q_{i,j} ← qaux_{i,0}

```

$\%A_{2CB} :=$ for $j \in 0..NoOfComb - 1$

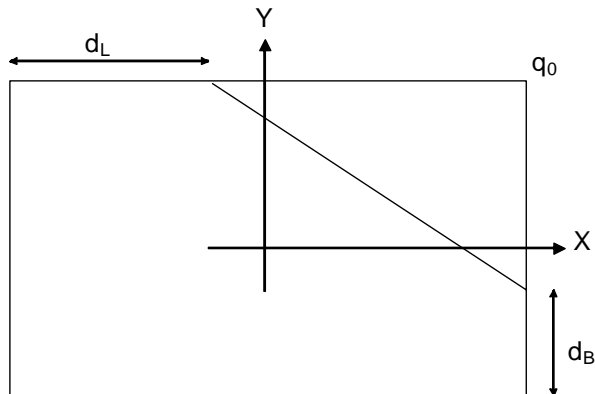
if $NBC_j = 2$

$\%A_j \leftarrow \%A_{2CB}(L_x, L_y, 1mm, 1mm, e_{x_j}, e_{y_j})$ if $\left| \frac{e_{y_j}}{L_y} \right| < \left| \frac{e_{x_j}}{L_x} \right|$

$\%A_j \leftarrow \%A_{2CB}(L_{x.2}, L_{y.2}, 1mm, 1mm, e_{x.2_j}, e_{y.2_j})$ otherwise

$\%A_j \leftarrow 0\%$ otherwise

ONE CORNERS IN BEARING



$$d_{y1,j} := 4 \cdot e_{y,j} - L_y \quad d_{x1,j} := 4 \cdot e_{x,j} - L_x \quad d_{y1,2,j} := 4 \cdot e_{y,2,j} - L_{y,2} \quad d_{x1,2,j} := 4 \cdot e_{x,2,j} - L_{x,2}$$

$q_{1CB} :=$ for $j \in 0..NoOfComb - 1$

if $\left| \frac{e_{y,j}}{L_y} \right| < \left| \frac{e_{x,j}}{L_x} \right|$

$$q_{1CB_{0,j}} \leftarrow \frac{1.5 \cdot P_j}{(L_y - 2 \cdot e_{y,j}) \cdot (L_x - 2 \cdot e_{x,j})}$$

$$q_{1CB_{1,j}} \leftarrow 0 \frac{\text{kgf}}{\text{cm}^2}$$

$$q_{1CB_{2,j}} \leftarrow 0 \frac{\text{kgf}}{\text{cm}^2}$$

$$q_{1CB_{3,j}} \leftarrow 0 \frac{\text{kgf}}{\text{cm}^2}$$

otherwise

$$q_{1CB_{0,j}} \leftarrow \frac{1.5 \cdot P_{2,j}}{(L_{y,2} - 2 \cdot e_{y,2,j}) \cdot (L_{x,2} - 2 \cdot e_{x,2,j})}$$

$$q_{1CB_{1,j}} \leftarrow 0 \frac{\text{kgf}}{\text{cm}^2}$$

$$q_{1CB_{2,j}} \leftarrow 0 \frac{\text{kgf}}{\text{cm}^2}$$

$$q_{1CB_{3,j}} \leftarrow 0 \frac{\text{kgf}}{\text{cm}^2}$$

$$\%A_{1CB} := \text{for } j \in 0..NoOfComb - 1$$

$$\left| \begin{array}{l} \frac{0.5 \cdot (L_y - d_{y1,j}) \cdot (L_x - d_{x1,j})}{A} \text{ if } \left| \frac{e_{y,j}}{L_y} \right| < \left| \frac{e_{x,j}}{L_x} \right| \\ \frac{0.5 \cdot (L_{y,2} - d_{y1,2,j}) \cdot (L_{x,2} - d_{x1,2,j})}{A} \text{ otherwise} \end{array} \right.$$

- Bearing pressure at remaining foundation corners

$$q_{bearingCorner} := \text{for } i \in 0..3$$

$$\text{for } j \in 0..NoOfComb - 1$$

$$\left| \begin{array}{l} q_{aux_{i,j}} \leftarrow q_{3CB_{i,j}} \text{ if } NBC_j = 3 \\ q_{aux_{i,j}} \leftarrow q_{4CB_{i,j}} \text{ if } NBC_j = 4 \\ q_{aux_{i,j}} \leftarrow q_{1CB_{i,j}} \text{ if } NBC_j = 1 \\ q_{aux_{i,j}} \leftarrow q_{2CB_{i,j}} \text{ if } NBC_j = 2 \end{array} \right.$$

$$\text{for } j \in 0..NoOfComb - 1$$

$$\left| \begin{array}{l} \text{if } \left| \frac{e_{y,j}}{L_y} \right| < \left| \frac{e_{x,j}}{L_x} \right| \\ \left| \begin{array}{l} q_{0,j} \leftarrow q_{aux_{0,j}} \\ q_{1,j} \leftarrow q_{aux_{1,j}} \\ q_{2,j} \leftarrow q_{aux_{2,j}} \\ q_{3,j} \leftarrow q_{aux_{3,j}} \end{array} \right. \\ \text{otherwise} \\ \left| \begin{array}{l} q_{0,j} \leftarrow q_{aux_{1,j}} \\ q_{1,j} \leftarrow q_{aux_{2,j}} \\ q_{2,j} \leftarrow q_{aux_{3,j}} \\ q_{3,j} \leftarrow q_{aux_{0,j}} \end{array} \right. \end{array} \right.$$

$$q$$

- % of footing in contact with soil

$$\%InContact := \text{for } j \in 0..NoOfComb - 1$$

$\%A_j$	$\leftarrow \%A_{3CB_j}$	if $NBC_j = 3$
$\%A_j$	$\leftarrow \%A_{4CB_j}$	if $NBC_j = 4$
$\%A_j$	$\leftarrow \%A_{1CB_j}$	if $NBC_j = 1$
$\%A_j$	$\leftarrow \%A_{2CB_j}$	if $NBC_j = 2$

- Maximum bearing pressure

$$q_{BearingMax} := \text{for } j \in 0..NoOfComb - 1$$

$$q_{BearingMax_j} \leftarrow \max(q_{bearingCorner}^{(j)})$$

- Overburden

$$\text{overburden} := \frac{\text{FootingWeight} + \text{SoilWeight}}{L_x \cdot L_y}$$

- Sliding

Sliding of foundations in response to design earthquake forces is usually very limited (fractions of a centimeter) and is typically considered as positive behavior. Sliding of foundations limits forces introduced into the structure, and therefore need not be checked. However, sliding of non anchored equipment and other nonstructural items could cause damage and should be checked.

$$FS_{sliding} = 2$$

$$= 1.5 \text{ (typically on Soil Reports)}$$

$$FS_{sliding_j} := \left| \begin{array}{l} \text{if } \left| \frac{e_{y_j}}{L_y} \right| < \left| \frac{e_{x_j}}{L_x} \right| \\ \left[\min \left[\frac{P_j \cdot \tan\left(\frac{2}{3} \cdot \phi\right) + (\%InContact_j \cdot L_x \cdot L_y) \cdot (0.80c)}{\sqrt{(V_{x_j})^2 + (V_{y_j})^2}}, 100 \right] \text{ if } \sqrt{(V_{x_j})^2 + (V_{y_j})^2} \neq 0 \right. \\ \left. 100 \text{ otherwise} \right. \\ \text{otherwise} \\ \left[\min \left[\frac{P_{2_j} \cdot \tan\left(\frac{2}{3} \cdot \phi\right) + (\%InContact_j \cdot L_{x,2} \cdot L_{y,2}) \cdot (0.80c)}{\sqrt{(V_{x,2_j})^2 + (V_{y,2_j})^2}}, 100 \right] \text{ if } \sqrt{(V_{x,2_j})^2 + (V_{y,2_j})^2} \neq 0 \right. \\ \left. 100 \text{ otherwise} \right. \end{array} \right.$$

- Overturning

Overturning of foundations in response to design earthquake loads is to be checked on an allowable stress basis using allowable stress load combinations. A factor of safety of 1.0 should be used considering only 90% of the dead load for resistance. The 0.9 factor accounts for uncertainty of the dead load and upward vertical acceleration.

FSOT = 1.2 ==> 25% of the soil compressed under the foundation
 = 1.5 ==> 50% of the soil compressed under the foundation
 = 2.0 ==> 75% of the soil compressed under the foundation
 = 3.0 ==> 100% of the soil compressed under the foundation

$$\text{FSOT}_{x_j} := \begin{cases} \text{if } \left| \frac{e_{y_j}}{L_y} \right| < \left| \frac{e_{x_j}}{L_x} \right| \\ \min \left(\frac{P_j \cdot L_y}{2 \cdot M_{xx_j}}, 100 \right) & \text{if } P_j \cdot M_{xx_j} > 0 \\ \min \left(-\frac{P_j \cdot L_y}{2 \cdot M_{xx_j}}, 100 \right) & \text{if } P_j \cdot M_{xx_j} < 0 \\ 100 & \text{otherwise} \\ \text{otherwise} \\ \min \left(\frac{P_{2_j} \cdot L_{y.2}}{2 \cdot M_{xx.2_j}}, 100 \right) & \text{if } P_{2_j} \cdot M_{xx.2_j} > 0 \\ \min \left(-\frac{P_{2_j} \cdot L_{y.2}}{2 \cdot M_{xx.2_j}}, 100 \right) & \text{if } P_{2_j} \cdot M_{xx.2_j} < 0 \\ 100 & \text{otherwise} \end{cases}$$

$$\text{FSOT}_{y_j} := \begin{cases} \text{if } \left| \frac{e_{y_j}}{L_y} \right| < \left| \frac{e_{x_j}}{L_x} \right| \\ \min \left(\frac{P_j \cdot L_x}{2 \cdot M_{yy_j}}, 100 \right) & \text{if } P_j \cdot M_{yy_j} > 0 \\ \min \left(-\frac{P_j \cdot L_x}{2 \cdot M_{yy_j}}, 100 \right) & \text{if } P_j \cdot M_{yy_j} < 0 \\ 100 & \text{otherwise} \\ \text{otherwise} \\ \min \left(\frac{P_{2_j} \cdot L_{x.2}}{2 \cdot M_{yy.2_j}}, 100 \right) & \text{if } P_{2_j} \cdot M_{yy.2_j} > 0 \\ \min \left(-\frac{P_{2_j} \cdot L_{x.2}}{2 \cdot M_{yy.2_j}}, 100 \right) & \text{if } P_{2_j} \cdot M_{yy.2_j} < 0 \\ 100 & \text{otherwise} \end{cases}$$

- Results

$$q_{\max} := \max(q_{\text{BearingMax}})$$

$$\% \text{InContact}_{\min} := \min(\% \text{InContact})$$

$$\text{FSsliding}_{\min} := \min(\text{FSsliding})$$

$$\text{FSOT}_{x.\min} := \min(\text{FSOT}_x)$$

$$\text{FSOT}_{y.\min} := \min(\text{FSOT}_y)$$

▣ Calculations

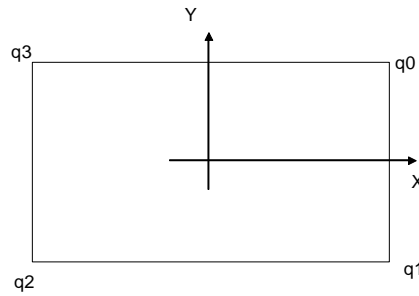
Pedestal coordinates

Pedestal No.	Joint No.	Coordinates [m]	
		X	Y
1	1979	-6,00	0,00
2	1998	0,00	0,00
3	1981	6,00	0,00

Forces and Moment at centroid of footing seal

Comb	Forces [tonf]			Moments [tonf-m]	
	P	Vx	Vy	Mxx	Myy
1	124,63	0,00	0,92	-0,41	0,00
2	119,49	-0,01	1,19	-0,57	0,00
3	52,58	-0,02	4,61	-2,73	0,00
4	124,65	-2,63	0,91	-0,43	13,09
5	134,31	0,05	-6,98	17,11	-0,09
6	124,64	28,74	1,05	-0,10	-141,35
7	115,84	-0,05	9,90	-19,63	0,08
8	124,63	-28,75	0,80	-0,72	141,35
9	133,42	0,04	-8,06	18,82	-0,08
10	66,75	-1,98	3,88	-2,29	9,82
11	73,99	0,02	-2,04	10,87	-0,06
12	66,73	21,55	3,98	-2,04	-106,02
13	60,14	-0,05	10,62	-16,69	0,06
14	66,73	-21,58	3,79	-2,50	106,01
15	73,33	0,02	-2,85	12,15	-0,06
16	74,80	-2,62	0,54	-0,27	13,09
17	84,46	0,05	-7,35	17,28	-0,09
18	74,78	28,75	0,68	0,07	-141,35
19	65,99	-0,05	9,53	-19,47	0,08
20	74,78	-28,75	0,43	-0,56	141,35
21	83,57	0,04	-8,42	18,98	-0,08
22	115,84	0,34	1,58	-0,54	19,59
23	48,93	0,32	5,00	-2,69	19,59
24	32,85	-1,73	3,94	-2,16	24,51
25	40,10	0,28	-1,98	11,00	14,63
26	32,84	21,80	4,04	-1,91	-91,33
27	26,24	0,21	10,68	-16,56	14,75
28	32,84	-21,32	3,85	-2,38	120,70
29	39,43	0,28	-2,79	12,27	14,63

Bearing pressure at remaining foundation corners and Maximum Bearing pressure



Comb	NBC	Bearing Corner [tonf/m ²]					qmax
		q0	q1	q2	q3		
1	4	2,79	2,75	2,75	2,79	2,79	
2	4	2,68	2,63	2,63	2,68	2,68	
3	4	1,29	1,05	1,05	1,29	1,29	
4	4	2,91	2,87	2,63	2,67	2,91	
5	4	3,74	2,22	2,22	3,75	3,75	
6	4	4,03	4,02	1,51	1,52	4,03	
7	4	3,45	1,70	1,70	3,45	3,45	
8	4	4,06	3,99	1,48	1,55	4,06	
9	4	3,80	2,13	2,13	3,80	3,80	
10	4	1,50	1,29	1,47	1,67	1,67	
11	4	2,13	1,16	1,16	2,13	2,13	
12	4	2,52	2,33	0,45	0,63	2,52	
13	4	2,08	0,59	0,60	2,08	2,08	
14	4	2,54	2,31	0,43	0,65	2,54	
15	4	2,17	1,09	1,09	2,17	2,17	
16	4	1,79	1,77	1,53	1,56	1,79	
17	4	2,64	1,11	1,11	2,65	2,65	
18	4	2,92	2,92	0,40	0,41	2,92	
19	4	2,33	0,60	0,60	2,33	2,33	
20	4	2,94	2,89	0,38	0,43	2,94	
21	4	2,70	1,01	1,01	2,70	2,70	
22	4	2,77	2,72	2,38	2,42	2,77	
23	4	1,38	1,14	0,79	1,03	1,38	
24	4	1,04	0,85	0,42	0,61	1,04	
25	4	1,25	0,27	0,53	1,51	1,51	
26	2	1,64	1,46	0,00	0,00	1,64	
27	2	0,63	0,00	0,00	2,68	2,68	
28	2	2,05	1,77	0,00	0,00	2,05	
29	4	1,29	0,20	0,46	1,55	1,55	

$$q_{\max} = 4.06 \frac{\text{tonnef}}{\text{m}^2}$$

$$q_{\text{net}} := q_{\text{all}} + \gamma_{\text{soil}} \cdot (\text{SoilAboveFooting} + \text{FootingThickness}) \quad q_{\text{net}} = 34.14 \frac{\text{tonn}}{\text{m}^2}$$

Footing in contact with soil, Sliding and Overturning Factors of Safety

Comb	NBC	%InContact	Factor of Safety		
			Sliding	OTx	OTy
1	4	100,00	54,54	100,00	100,00
2	4	100,00	40,69	100,00	100,00
3	4	100,00	4,61	100,00	28,93
4	4	100,00	18,12	100,00	71,42
5	4	100,00	7,77	100,00	11,77
6	4	100,00	1,75	100,00	6,61
7	4	100,00	4,73	100,00	8,85
8	4	100,00	1,75	100,00	6,61
9	4	100,00	6,69	100,00	10,64
10	4	100,00	6,20	51,00	43,70
11	4	100,00	14,63	100,00	10,21
12	4	100,00	1,23	49,16	4,72
13	4	100,00	2,29	100,00	5,41
14	4	100,00	1,23	39,96	4,72
15	4	100,00	10,39	100,00	9,05
16	4	100,00	11,28	100,00	42,86
17	4	100,00	4,64	100,00	7,33
18	4	100,00	1,05	100,00	3,97
19	4	100,00	2,80	100,00	5,08
20	4	100,00	1,05	100,00	3,97
21	4	100,00	4,01	100,00	6,60
22	4	100,00	29,04	100,00	44,36
23	4	100,00	3,95	27,25	18,74
24	4	100,00	3,09	22,77	10,05
25	4	100,00	8,09	20,56	5,47
26	2	94,17	0,60	25,79	2,70
27	2	62,41	0,99	13,34	2,38
28	2	76,21	0,61	20,71	2,04
29	4	100,00	5,69	20,22	4,82

$$\%InContact_{min} = 62.41 \%$$

$$FS_{sliding}_{min} = 0.60$$

$$FSOT_{x.min} = 13.34$$

$$FSOT_{y.min} = 2.04$$

4.0 RESULTS:

Maximum Bearing pressure	$\text{if}(\max(q_{\text{BearingMax}}) \geq q_{\text{net}}, "X", "ok") = "ok"$
Footing in contact with soil	$\text{if}(\min(\% \text{InContact}) < \% \text{InContact}_{\text{all}}, "X", "ok") = "ok"$
Sliding Factor of Safety	$\text{if}(\min(\text{FS}_{\text{sliding}}) < \text{FS}_{\text{sliding}_{\text{all}}}, "X", "ok") = "X"$
Overturning Factor of Safety	$\text{if}(\min(\text{FSOT}_x) < \text{FSOT}_{\text{all}}, "X", "ok") = "ok"$ $\text{if}(\min(\text{FSOT}_y) < \text{FSOT}_{\text{all}}, "X", "ok") = "ok"$

5.0 SKETCHES:

