

Description

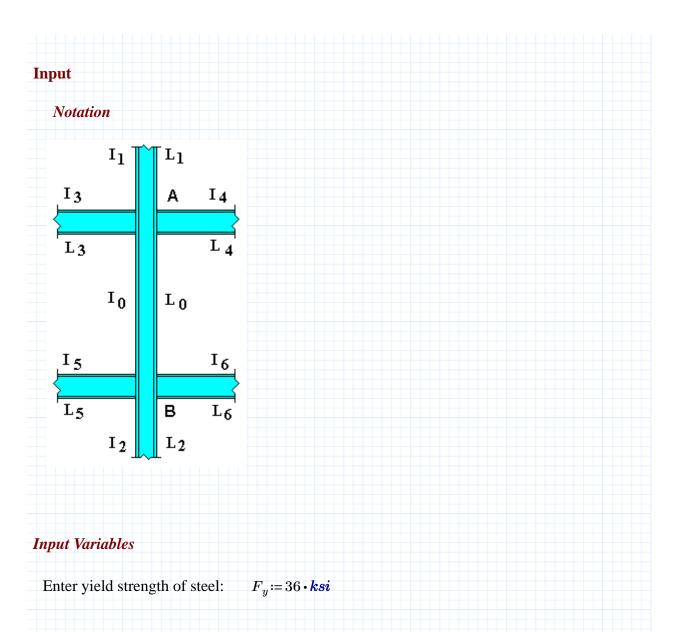
In frames where lateral stability is dependent upon the bending stiffness of rigidly connected beams and columns the effective length of compression members must be determined. The effective length method uses K factors to equate the strength of a framed compression element of length L to an equivalent pin-ended member of length KL subject to axial load only. After preliminary trial members have been determined, the alignment chart of AISC Specifications Commentary C-C2 may be used to determine K values. The K values determined from the alignment chart are based on the assumption of purely elastic column behavior and are referred to as elastic K factors. However, most steel columns behave inelastically and the elastic K factors may be reduced using the stiffness reduction factors of the AISC Manual, Table A (Section 3, page 8).

This application computes the stiffness reduction factors for inelastic behavior (Table A, page 3-8 of the AISC Manual), the stiffness ratios at the ends of the column (G values), and the effective length factor k for sidesway permitted. Mathcad's **root** function and solve block are used to compute the stiffness reduction factors and to solve the transcendental equation for effective length factors, eliminating the need to use the alignment chart in the AISC Commentary. If the user does not require the inelastic effective length factors, <u>Section 5.5</u> may be used to compute elastic effective length factors.

The required input includes the column axial loads on the column being examined and on the columns above and below this column, the cross section area and radius of gyration of the column sections, the moments of inertia and member lengths of all members rigidly connected at each end of the column, and the type of column base when applicable.

A summary of input and computed variables is shown on pages 7 and 8.

Reference: AISC "Manual of Steel Construction — Allowable Stress Design" June 1, 1989



Enter axial load, area of the column section and the radius of gyration in the plane of bending for the column under consideration, the column above, and the column below, in sequence starting with subscript 0 for the column under consideration.

Column axial load:

 $P_{0} := 560 \cdot kip$ $P_{1} := 510 \cdot kip$ $P_{2} := 610 \cdot kip$

Column section area:

 $A_{0} := 31.2 \cdot in^{2}$ $A_{1} := 31.2 \cdot in^{2}$ $A_{2} := 39.9 \cdot in^{2}$

Radius of gyration in the plane of bending:

$r_{b_0} \! \coloneqq \! 5.47 \cdot \! in$	$r_{b_1} = 5.47 \cdot in$	$r_{b_2} \coloneqq 5.58 \cdot in$
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Enter moments of inertia and lengths of the members framing into the joints at the top and bottom of the column under consideration. Top and bottom joints are designated A and B, respectively. The first I and L entered must be for the column under consideration.

[933]	[15]	1st row \leftarrow column at story
933	15	2nd row \leftarrow column above
1240	15	3rd row \leftarrow column below
$I \coloneqq 375 \cdot in^4$	$L \coloneqq 20 \cdot ft$	4th row \leftarrow girder top
0	0	5th row \leftarrow girder top
375	20	6th row \leftarrow girder below
	[0]	7th row \leftarrow girder below

Define the variable "Base" as 0 if lower end is pinned, 1 if fixed and 2 if framed:

 $Base \coloneqq 2$

Computed Variables

fa	axial compression stress
Cc	column slenderness ratio separating elastic and inelastic buckling
	(see AISC Specification, Eq. (E2-1))
Fa	allowable axial stress determined by AISC Specification, Eq. (E2-1)
SR	slenderness ratios SR at which axial stress equals the allowable stress determined by
	AISC Specification, Eq. (E2-1)
F'e	Euler's stress divided by a factor of safety (AISC Specification, Sect. H1)
SRF	stiffness reduction factor for inelastic behavior, equal to axial stress divided by Euler's
	stress calculated at the slenderness ratio in the plane of bending at which axial stress
	equals the allowable axial stress
Ga,Gb	ratios of the sum of the column stiffnesses multiplied by the inelastic stiffness
	reduction factor, to the sum of the girder stiffnesses at top and bottom (joints A and B,
	respectively) of the column under consideration
K	effective length factor reduced for inelastic column behavior

Calculations

Axial stress:

$$i := 0..2$$
 $f_{a_i} := \frac{P_i}{A_i}$ $f_a = \begin{bmatrix} 17.949 \\ 16.346 \\ 15.288 \end{bmatrix} ksi$

Modulus of elasticity of steel:

$$E \coloneqq 29000 \cdot ksi$$

Column slenderness ratio separating elastic and inelastic buckling (AISC Specification, Eq. (E2-1)):

$$C_c \coloneqq \sqrt{\frac{2 \cdot \pi^2 \cdot E}{F_y}} \qquad \qquad C_c = 126.099$$

Allowable axial stress determined by AISC Specification, Eq. (E2-1) expressed as a function of the larger slenderness ratio SR:

$$F_a(SR) \coloneqq \frac{\left(1 - \frac{SR^2}{2 \cdot C_c^2}\right) \cdot F_y}{\frac{5}{3} + \frac{3 \cdot SR}{8 \cdot C_c} - \frac{SR^3}{8 \cdot C_c^3}}$$

Function for determining the value of SR at which axial stress equals the allowable stress determined by AISC Specification, Eq. (E2-1):

$$f(SR,i) \coloneqq \left(f_{a_i} - F_a(SR)\right)$$

Guess value of slenderness ratio:

$$SR \coloneqq C_c$$

Slenderness ratios SR at which axial stress equals the allowable stress determined by AISC Specification, Eq. (E2-1):

$$SR_i = \operatorname{root}(f(SR,i),SR)$$

$$SR^{\mathrm{T}} = [54.471 \ 70.811 \ 80.601]$$

Euler's stress divided by a factor of safety (AISC Specification, Sect. H1):

$$F'_{e} \coloneqq \frac{12 \cdot \pi^{2} \cdot \vec{E}}{23 \cdot SR^{2}} \qquad \qquad F'_{e}^{T} = [50.328 \ 29.782 \ 22.986] \ ksi$$

Stiffness reduction factor for inelastic behavior, equal to axial stress divided by Euler's stress calculated at the slenderness ratio in the plane of bending at which axial stress equals the allowable axial stress. When the slenderness ratio is greater than Cc, there is no stiffness reduction.

Stiffness reduction factors:

$$i := 0..2$$
 $SRF_i := if \left(SR_i < C_c, \frac{f_{a_i}}{F'_{e_i}}, 1 - \frac{f$

 $SRF^{\mathrm{T}} = [0.357 \ 0.549 \ 0.665]$

Ratios GA and GB, the sum of the column stiffnesses multiplied by the inelastic stiffness reduction factor, to the sum of the girder stiffnesses at top and bottom (joints A and B, respectively) of the column under consideration:

$$G_{A} \coloneqq \frac{I_{0}}{I_{0}} + SRF_{1} \cdot \frac{I_{1}}{L_{1}} = 3.004$$

$$G_{A} \coloneqq \frac{I_{0}}{I_{3}} + I_{3} + (I_{4} > 0 \cdot in^{4}) \cdot \frac{I_{3}}{L_{3}} = 3.004$$

 $SRF_0 \cdot \frac{I_0}{L_0} + SRF_2 \cdot \frac{I_2}{L_2}$ $G_B := if | Base = 0, 10, if | Base = 1, 1, -$ =4.115

$$I_{5} > 0 \cdot in^{4} \cdot \frac{I_{5}}{L_{5}} + (I_{6} > 0 \cdot in^{4} \cdot \frac{I_{5}}{L_{5}} ||$$

Effective length factor for Columns with sidesway uninhibited:

(The equation shown within the Mathcad solve block is the equation solved by the alignment chart shown in the AISC Specification Commentary, Section C-C2.)

K factor, reduced for inelastic column behavior, as applicable:

K = 1.938

Summary

Yield	strength of steel:	
TICIU	strength of steel.	

 $F_y = 36 \ ksi$

Variable "Base" equal to 0 for pinned base, 1 for fixed base, and 2 for framed lower end:

Base = 2

Column axial load:

Cross section area of column:

at story \rightarrow 1st row	[560]	[31.2]
story above \rightarrow 2nd row	P = 510 kip	$A = 31.2 in^2$
story below \rightarrow 3rd row	[610]	[39.9]

Radius of gyration in the plane of bending of the column section:

at story \rightarrow 1st row	[5.47]
story above \rightarrow 2nd row	$r_b = 5.47 in$
story below \rightarrow 3rd row	

Column slenderness ratio separating elastic and inelastic buckling (AISC Specification, Eq. (E2-1)):

 $C_c \!=\! 126.099$

Stifferen and wation footons (for	[0.357]	1st row \leftarrow at story
Stiffness reduction factors: (for inelastic column behavior)	SRF = 0.549	2nd row \leftarrow story above
merastic column benavior)	$\lfloor 0.665 \rfloor$	3 rd row \leftarrow story below

Stiffness factors GA and GB reduced by stiffness reduction factor SRF when SR < Cc:

$$G_A = 3.004$$

 $G_B = 4.115$

Column and girder lengths and moments of inertia: (Enter member size designations.)

		W12x106	
1st row \leftarrow W12x106	[933]	[15]	1st row \leftarrow column at story
2nd row \leftarrow W12x106	933	15	-2 nd row \leftarrow column above
$3rd row \leftarrow W12x136$	$1.24 \cdot 10^{3}$	15	$3rd row \leftarrow column below$
4th row \leftarrow W16x26	$I = 375$ in^4	$L = 20 \mid ft$	4th row \leftarrow girder top
5th row \leftarrow	0	0	5th row \leftarrow girder top
6th row \leftarrow W16x26	375		6th row \leftarrow girder below
7th row \leftarrow		[0]	7th row \leftarrow girder below

K factor, reduced for inelastic column behavior when applicable:

K = 1.938

