

Calculation applies to
 ADN8UP SADNUP upper radial connector rotating bending qualification test:
 100862958; ET201009263

$$\rho := .25 \cdot \frac{\text{lb}}{\text{in}^3}$$

$$A_a := 43 \cdot \text{in}^2$$

$$A_b := 19.8 \cdot \text{in}^2$$

$$E := 200 \cdot \text{GPa} = 2.901 \times 10^7 \text{ psi}$$

$$q_a := \rho \cdot A_a \cdot \frac{\text{lb}}{\text{lbm}} = 10.75 \cdot \frac{\text{lb}}{\text{in}}$$

$$I_a := 190 \cdot \text{in}^4$$

$$q_b := \rho \cdot A_b \cdot \frac{\text{lb}}{\text{lbm}} = 4.95 \cdot \frac{\text{lb}}{\text{in}}$$

$$I_b := 50.6 \cdot \text{in}^4$$

$$L_a := 62 \cdot \text{in}$$

$$L_b := 99 \cdot \text{in}$$

$$x_P := 206 \cdot \text{in} \quad P := 12900 \cdot \text{lb}$$

$$x_2 := x_P + 40 \cdot \text{in} = 246 \cdot \text{in}$$

$$x_D := 202 \cdot \text{in}$$

$$x_{\text{end}} := 263 \cdot \text{in}$$

$$\text{SumR} := P + q_a \cdot L_a + q_b \cdot L_b + q_a \cdot (x_{\text{end}} - L_a - L_b) = 1.515 \times 10^4 \cdot \text{lb}$$

$$R_2 := \left[P \cdot x_P + q_a \cdot L_a \cdot \frac{L_a}{2} + q_b \cdot L_b \cdot \left(L_a + \frac{L_b}{2} \right) \dots \right] \cdot \frac{1}{x_2} = 12.053 \cdot \text{kip}$$

$$\left[+ q_a \cdot (x_{\text{end}} - L_a - L_b) \cdot \left(L_a + L_b + \frac{x_{\text{end}} - L_a - L_b}{2} \right) \right]$$

$$R_1 := \text{SumR} - R_2 = 3.1 \cdot \text{kip}$$

$$q(x) := -q_a \cdot (1 - \Phi(x - L_a)) - q_b \cdot (\Phi(x - L_a) - \Phi(x - L_a - L_b)) - q_a \cdot \Phi(x - L_a - L_b)$$

$$V_1(x) := \int_0^x q(x) dx + R_1 - P \cdot (x > x_P) + R_2 \cdot (x > x_2)$$

$$M_1(x) := \int_0^x V_1(x) dx$$

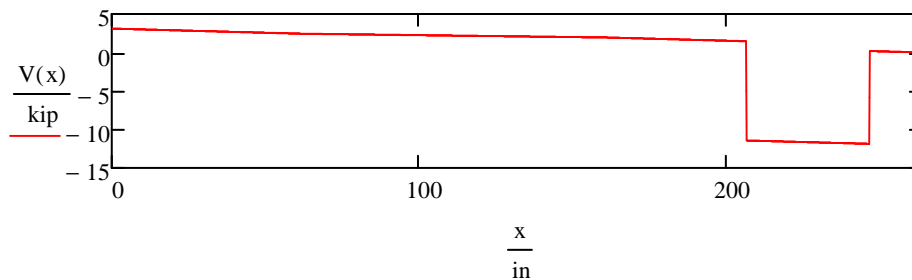
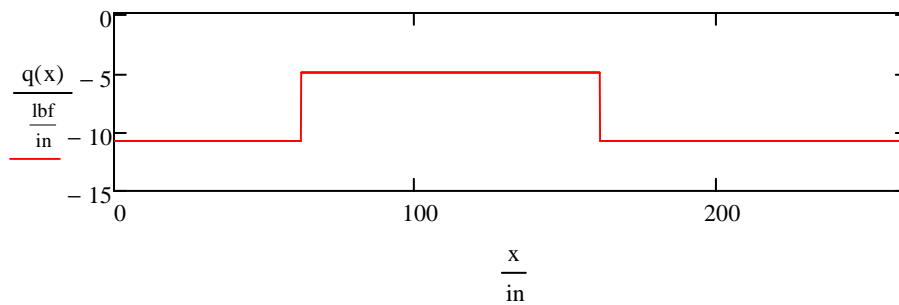
$$M_1(250 \cdot \text{in}) =$$

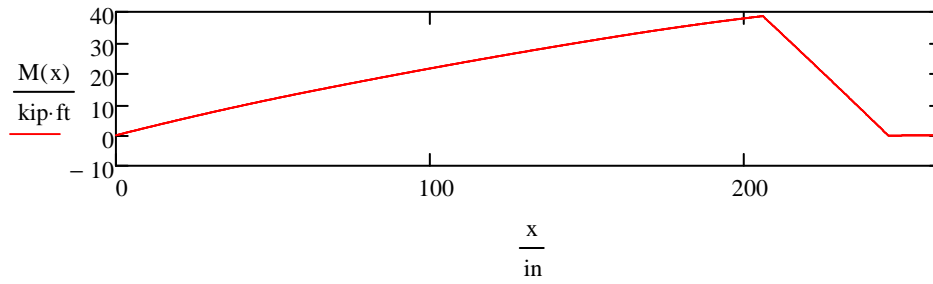
$$V(x) := -q_a \cdot [x - (x - L_a) \cdot \Phi(x - L_a)] - q_b \cdot [(x - L_a) \cdot \Phi(x - L_a) - (x - L_a - L_b) \cdot \Phi(x - L_a - L_b)] \dots \\ + -q_a \cdot (x - L_a - L_b) \cdot \Phi(x - L_a - L_b) + R_1 - P \cdot \Phi(x - x_p) + R_2 \cdot \Phi(x - x_2)$$

$$M(x) := -q_a \cdot \left[\frac{1}{2} x^2 - \frac{1}{2} (x - L_a)^2 \cdot \Phi(x - L_a) \right] \dots \\ + -q_b \cdot \left[\frac{1}{2} (x - L_a)^2 \cdot \Phi(x - L_a) - \frac{1}{2} (x - L_a - L_b)^2 \cdot \Phi(x - L_a - L_b) \right] \dots \\ + -q_a \cdot \frac{1}{2} (x - L_a - L_b)^2 \cdot \Phi(x - L_a - L_b) \dots \\ + R_1 \cdot x - P \cdot (x - x_p) \cdot \Phi(x - x_p) + R_2 \cdot (x - x_2) \cdot \Phi(x - x_2)$$

$$M(x_D) = 38.229 \text{ kip} \cdot \text{ft}$$

$$x := 0, 0.1 \cdot \text{in} \dots x_{\text{end}}$$

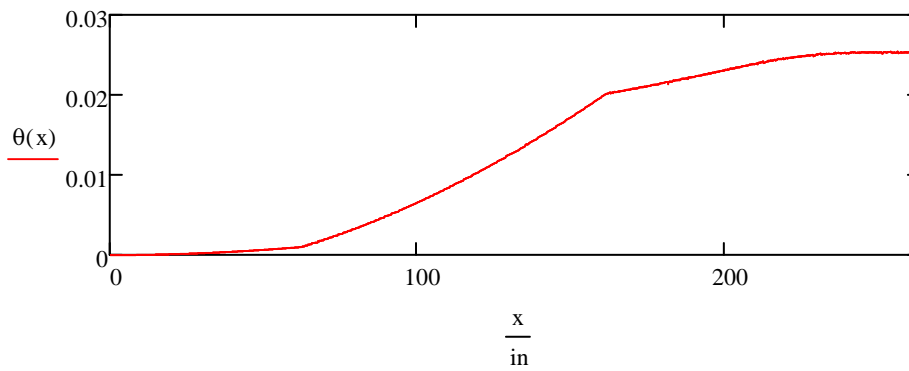
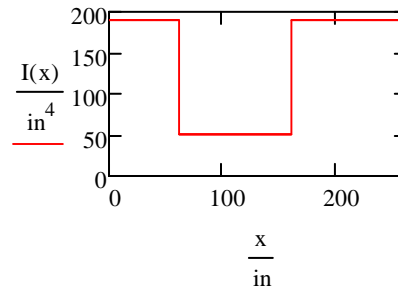




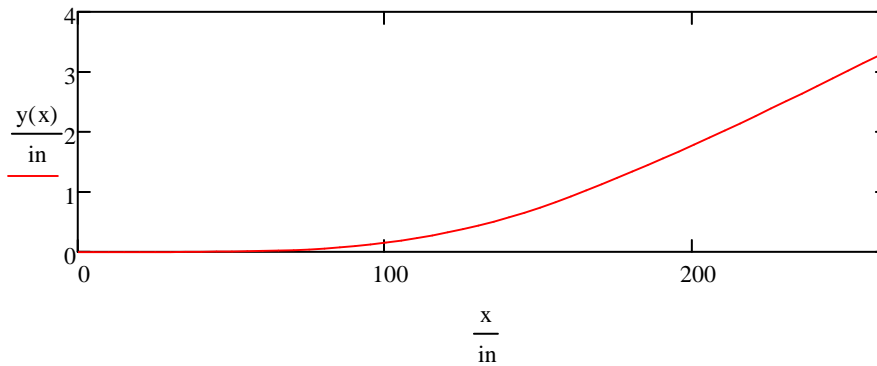
$$I(x) := \text{if}(L_a < x < L_a + L_b, I_b, I_a)$$

$$\theta(x) := \int_0^x \frac{1}{E \cdot I(x)} M(x) dx$$

$$y(x) := \int_0^x \theta(x) dx$$



$$x := 0, 5 \cdot \text{in} .. x_{\text{end}}$$



To simplify setup, let the drive bearing and far-end support the roll assembly offset from the floor. Apply load using the bending deflector and measure the displacement at the bending deflector.

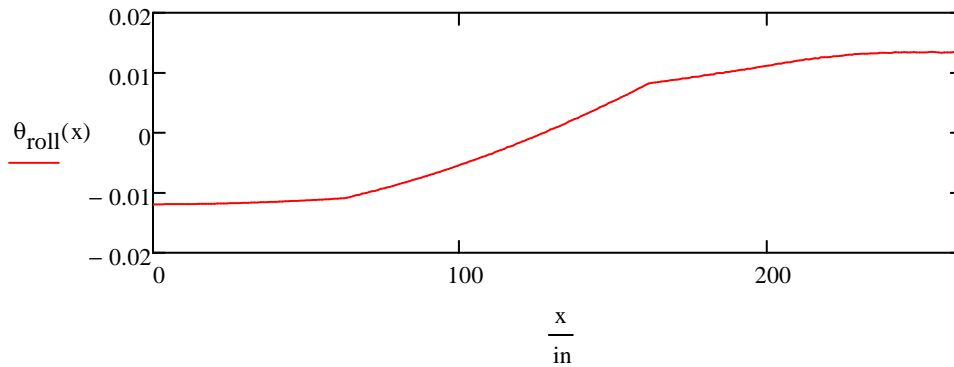
$$\theta_0 := \frac{y(x_2)}{x_2} = 0.012$$

$$\theta_{\text{roll}}(x) := \theta(x) - \theta_0$$

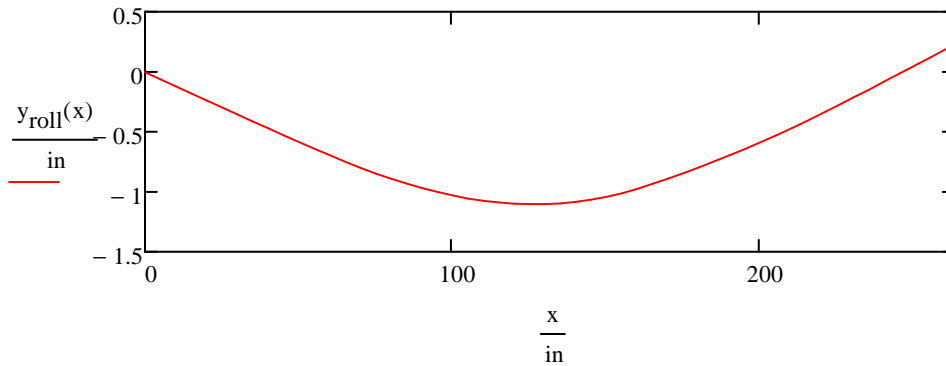
$$y_{\text{roll}}(x) := y(x) - x \cdot \theta_0$$

$$\min(y_{\text{roll}}(x), x, 0, x_{\text{end}}) =$$

$$x := 0, 1 \cdot \text{in} \dots x_{\text{end}}$$



$$x := 0, 5 \cdot \text{in} \dots x_{\text{end}}$$



$$y_{\text{roll}}(x_D) = -0.561 \text{ in}$$

$$y_{\text{roll}}(125 \cdot \text{in}) = -1.101 \text{ in}$$